# Viscosity of Molten Rare Earth Metal Trichlorides II. Cerium Subgroup

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The kinematic viscosity of molten LaCl<sub>3</sub>, CeCl<sub>3</sub>, PrCl<sub>3</sub>, NdCl<sub>3</sub>, and SmCl<sub>3</sub> was measured directly by using a capillary viscometer made of quartz and a transparent electric furnace. Viscosity of molten PmCl<sub>3</sub> and EuCl<sub>3</sub> was estimated using common tendencies in the lanthanides row. The dynamic viscosity was computed by using the most reliable density data taken from literature. The viscosity of molten lanthanides trichlorides at the same temperature changes slightly within a cerium lanthanides subgroup. Molten EuCl<sub>3</sub> perhaps has abnormally low viscosity.

Key words: Viscosity; Molten Salts; Rare Earths; Chlorides.

### 1. Introduction

The viscosity of molten rare earth chlorides (LnCl<sub>3</sub>) and their binary mixtures with alkali chlorides are poorly known to date. The data available in literature are very fragmentary and contradictory [1].

Viscosity is a very important property of liquids both from practical and theoretical points of view. The use of molten chloride salts has been proposed in the field of nuclear fuel cycle based on pyrochemistry [2] and the transmutation process of minor actinides with proton accelerator [3]. Physical and chemical properties of molten salts must be known for the development of those technologies. From the other hand, knowledge of viscosity gives substantial information on the structure of liquids [4].

The present paper is a continuation of our first publication [5], devoted to systematic study of viscosity of molten LnCl<sub>3</sub>.

Viscosity measurements at high temperatures (above 700-900 K) are a difficult experimental field. In the case of molten rare earth halides the most important and complicated problem is the preparation of oxichlorides-free salts and keeping melt under study free from contacts with oxidants or moisture.

In this work particular attention was paid to the preparation of anhydrous salts. In order to exclude any contact of  $LnCl_3$  with atmosphere during the measurements, completely closed viscometers were used.

The kinematic viscosities of molten LaCl<sub>3</sub>, CeCl<sub>3</sub>, PrCl<sub>3</sub>, NdCl<sub>3</sub>, and SmCl<sub>3</sub> were studied by using a capillary viscometer. Temperature range of measurements was from the melting point to typically 1170-1190 K. The viscosity of molten PmCl<sub>3</sub> and EuCl<sub>3</sub> was estimated using common tendencies in the lanthanides row. The dynamic ( $\eta$ ) and molar viscosity ( $\eta_M$ ) were calculated from the measured kinematic viscosity ( $\nu$ ) and the density (d) data recommended in [6, 7].

#### 2. Experimental

### 2.1. Apparatus

A capillary viscometer entirely made of quartz was used in the present study. It consists of an outside tube sealed hermetically and a capillary, 0.4 mm inner diameter, placed inside. Upwardly, the capillary was connected with timing bulb approximately 3-4 ml capacity. An outlet of special shape was attached to the capillary at the bottom in order to compensate surface ten-

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sion forces, connected with meniscus. For more details, see [5, 8].

### 2.2. Determination of the Viscometer Constants

Before each measurement the viscometer was calibrated and the constants  $C_1$  and  $C_2$  in the following equation were precisely determined [8]:

$$v = C_1 t - C_2 / t. (1)$$

In general,  $C_2/t$  is small as compared with  $C_1t$ . Usually  $C_2/t$  does not exceed 2% of  $C_1t$ , but in rare cases can reach 5-10 %. The choice of a suitable calibration liquid is rather important for reliable determination of the  $C_1$  and  $C_2$  constants. Distilled water is the best choice because the viscosity and density of water are most precisely known compared with those for all other liquids. Water covers a wide range of kinematic viscosity which is nearly the same as that of the melts under investigation. The main argument against water is essential (several hundred degrees) difference between the calibration and the working temperature. But because of the very small quartz temperature expansion coefficient  $(5.8 \cdot 10^{-7} \text{ k}^{-1} \text{ [9]})$  the error due to thermal quartz expansion is negligible (less than 0.15%).

For determination of the viscometer constants, the flow time of distilled water was measured in a water thermostat over the temperature range 275-338 K with increments of about 10 K. A typical result is shown in Figure 1. The constants are calculated with the least-squared method using (2) for viscosity of water:

$$lg(\mathbf{v}) = -5.613291 + \frac{4325.4932}{T} - \frac{1354943.57}{T^2} + \frac{166934200}{T^3}.$$
(2)

The resulting  $C_1$  and  $C_2$  values are shown in Figure 1 too. Equation (2) is an approximation of distilled water viscosity data from [9].

## 2.3. Chemicals

Anhydrous lanthanum, cerium, and praseodymium trichlorides were obtained by dehydration of  $LaCl_3 \cdot 7H_2O$ ,  $CeCl_3 \cdot 7H_2O$ , and  $PrCl_3 \cdot 7H_2O$ , respectively. Anhydrous NdCl<sub>3</sub> and SmCl<sub>3</sub> were synthesized from the corresponding oxides. The initial salt



Fig. 1. Calibration of the viscometer with distilled water. Cell 53-A.  $\nu$ : kinematic viscosity of water; t: time in s.

and oxides were Soekawa Chemicals (Japan) 99.9% materials. The oxides were dissolved in concentrated HCl with subsequent crystallization of the hydrates  $LnCl_3 \cdot 6H_2O$ :

$$Ln_2O_3 + 6HCl_{acid} = 2LnCl_3 + 3H_2O.$$
 (3)

Dehydration of crystalline hydrates was carried out by heating in a flow of dry N<sub>2</sub> up to 130-180 °C (depends on the element). The resulting product was LnCl<sub>3</sub> · (1-2)H<sub>2</sub>O. Then the N<sub>2</sub> flow was replaced with a flow of dry HCl<sub>(gas)</sub>, and the salt was further heated up to melting. It is very important to carry out the dehydration slowly to prevent the formation of oxichlorides. Finally, the rare earth chlorides were distilled under vacuum (~ 1 Pa) and subsequently were handled under inert atmosphere with a water content of 1-2 ppm.

No insoluble matter was found in the course of dissolving the chlorides in distilled water. By the solubility tests [5, 10] the quality of each lot of LnCl<sub>3</sub> was controlled. About 0.5 g of the salt was dissolved in 3-4 cm<sup>3</sup> distilled water. The solution is absolutely transparent or has a weak opalescence when oxichlorides are absent. In several cases, especially for the heavy lanthanides, hydrolysis occurs during the dissolution with hydroxide formation. In this case, 1-2 drops of concentrated HNO<sub>3</sub> were enough to suppress hydrolysis. If the solution still remained opaque after 2 drops of HNO<sub>3</sub>, the content of oxichlorides was considered to be too high and the product was used as a row material. For more details, see [5]. A. Potapov and Y. Sato · Viscosity of Molten Rare Earth Metal Trichlorides

#### 3. Results and Discussion

The experimental kinematic viscosity values of molten LaCl<sub>3</sub>, CeCl<sub>3</sub>, PrCl<sub>3</sub>, and NdCl<sub>3</sub> are shown in Figure 2. In all cases viscosities decrease with temperature increases. The viscosities of molten cerium, praseodymium, neodymium, and samarium chlorides are very close to each other. For example maximum difference between them does not exceed 2.2% at 800 °C and 5.3% at 900 °C. The kinematic viscosity of lanthanide chlorides as a function of temperature is adequately approximated by the equation

$$\ln(\nu) = \ln(\nu_0) + \frac{E_A}{R \cdot T},\tag{4}$$

where v is the kinematic viscosity, and  $E_A$  is the activation energy of viscous flow.

The coefficients  $v_0$  and  $E_A$  are summarized in Table 1.

The dependence of kinematic viscosities on reverse radius of lanthanide cation at 1073 and 1173 K is



Fig. 2. Kinematic viscosities of molten rare earth chlorides of cerium subgroup.

Table 1. Kinematic viscosity  $(\ln(v) = \ln(v_0) + E_A/RT)$  of molten rare earth chlorides. Total error does not exceed  $\pm$  3%, with the exception of EuCl<sub>3</sub>, for which error estimation is 5–6%.  $R = 8.31441 \text{ J}/(\text{K} \cdot \text{mol})$ , T [K].

Salt	$\ln(v_0)$	$E_{\rm A}$ , [J/mol]	$v \cdot 10^{-6}$ , [m <sup>2</sup> /s]		$\Delta T$ , [K]
	. ,		1073 K	1173 K	
LaCl <sub>3</sub>	-3.5115	35051	1.517	1.086	1140-1196
CeCl <sub>3</sub> [5]	-3.2396	31788	1.381	1.019	1090 - 1177
PrCl <sub>3</sub>	-3.5051	34087	1.371	0.990	1064 - 1185
NdCl <sub>3</sub> [5]	-3.4252	33605	1.406	1.020	1025 - 1151
PmCl <sub>3</sub>	-3.572	35000	1.438	1.029	_
SmCl <sub>3</sub> [5]	-4.0118	38823	1.404	0.969	948-1094
EuCl <sub>3</sub>	-3.704	35000	1.25	0.895	-

shown in Figure 3. In such coordinates, the tendency of viscosity variation in a row of lanthanides is clearer.

The dynamic viscosity  $(\eta)$  was calculated according to (5):

$$\eta = \mathbf{v} \cdot \mathbf{d},\tag{5}$$

where *d* is the density of the melt.

For computing the dynamic viscosity, the densities of molten LnCl<sub>3</sub> recommended in [6, 7] were used. The densities published in [6, 7] are a complete and self-consistent set of data and therefore the data are preferable. The results are summarized in Table 2 and are juxtaposed with literature data in Figures 4-6. For molten CeCl<sub>3</sub>, NdCl<sub>3</sub>, and SmCl<sub>3</sub> such comparison was made earlier [5]. The coefficients in dynamic viscosity equations for molten CeCl<sub>3</sub>, NdCl<sub>3</sub>, and SmCl<sub>3</sub> given in Table 2 slightly differ from the data presented in paper [5] as the more reliable density data were used.

Our viscosity data on LaCl<sub>3</sub> are the lowest ones (see Figure 3). At 1173 K the difference with data [11, 12] is approximately 6.3% and  $\approx 8.4\%$  with data [13].



Fig. 3. Kinematic viscosities of molten LnCl<sub>3</sub> vs.  $1/r_{Ln^{3+}}$ .

Table 2. Dynamic viscosity  $(\ln(\eta) = \ln(\eta_0) + E_A/RT)$  of molten rare earth chlorides. Total error does not exceed  $\pm 4\%$ , except of EuCl<sub>3</sub>.  $R = 8.31441 \text{ J}/(\text{K} \cdot \text{mol})$ , T [K].

Salt	$\ln(\eta_0)$	$E_{\rm A}$ , [J/mol]	$\eta$ , [mPa · s]		$\Delta T$ , [K]
			1073 K	1173 K	
LaCl <sub>3</sub>	-2.6050	37455	4.918	3.438	1140-1196
CeCl <sub>3</sub>	-2.3488	34420	4.521	3.254	1090-1177
PrCl <sub>3</sub>	-2.6029	36637	4.496	3.168	1064-1185
NdCl <sub>3</sub>	-2.4788	35875	4.673	3.317	1025-1151
PmCl <sub>3</sub>	-2.6366	37389	4.729	3.309	_
SmCl <sub>3</sub>	-3.0131	40837	4.776	3.233	948-1094
EuCl <sub>3</sub>	-2.6954	36972	4.256	2.989	-



Fig. 4. Dynamic viscosity of molten LaCl<sub>3</sub>. All data available.



Fig. 5. Dynamic viscosity of molten PrCl<sub>3</sub>. All data available.



Fig. 6. Molar viscosity of molten LnCl<sub>3</sub> of cerium subgroup.

One of the possible reasons of the discrepancy is the postmelting effect, which is considered below. More than 60% deviation from [14, 15] is undoubtedly the consequence of inadequate LaCl<sub>3</sub> preparation. The presence of fine powder of insoluble LaOCl increases total viscosity.

The somewhat lower viscosity of  $PrCl_3$  according to Cho and Kuroda [16] is probably a consequence of some defect of his measuring procedure.

Similar to molar conductivity the molar viscosity  $(\eta_M)$  is a property normalized to the same number (1 mole) of particles [4, 5, 17–19]. In this sense the molar viscosity is the most correct characteristic for comparison of different substances.

Molar viscosity is the energy which dissipates a flow of one mole of liquid running with unit velocity gradient owing to internal friction forces.

It was calculated according to

$$\eta_{\rm M} = \eta \cdot V_{\rm m},\tag{6}$$

where  $V_{\rm m}$  is the molar volume.

Since  $\eta = v \cdot d$  and  $V_m = M/d$ , another expression is obtained for molar viscosity:

$$\eta_{\rm M} = v \cdot M, \tag{7}$$

where *M* is the molar mass.

Until now there is no conventionally accepted unit for  $\eta_{\rm M}$ . According to (7) the unit is

$$[\eta_M] = \frac{\mathrm{m}^2}{\mathrm{s}} \cdot \frac{\mathrm{kg}}{\mathrm{mol}} = \frac{\mathrm{kg} \cdot \mathrm{m}^2}{\mathrm{s} \cdot \mathrm{mol}}.$$
(8)

Since  $J = kg \cdot m^2/c^2$ 

$$\eta_{\rm M}] = J \cdot s/{\rm mol.} \tag{9}$$

In the present paper, second version (9) is used.

Molar viscosities of investigated LnCl<sub>3</sub> are summarized in Table 3 and are plotted as  $\eta_{\rm M}$  vs.  $1/r_{\rm Ln^{3+}}$ in Figure 6. Generally the viscosity slightly increases within the cerium subgroup; however, the viscosity values for LaCl<sub>3</sub> and EuCl<sub>3</sub> lie out of the main tendency.

LaCl<sub>3</sub>. The surprising thing is that the viscosity of molten LaCl<sub>3</sub> is higher than the viscosities of all chlorides from CeCl<sub>3</sub> to SmCl<sub>3</sub>. The nature of this abnormality is not yet entirely known. At the same time,

Table 3. Molar viscosity  $(\ln(\eta_M) = \ln(\eta_{M0}) + E_A/RT)$  of molten rare earth chlorides.  $R = 8.31441 \text{ J/(K} \cdot \text{mol}), T$  [K].

Salt	$\ln(\eta_{M0})$	$E_{\rm A}$ , [J/mol]	$\eta_{\rm M} \cdot 10^9$ ,	[J · s/mol]	$\Delta T$ , [K]
			1073 K	1173 K	
LaCl <sub>3</sub>	1.9908	35051	372.1	266.2	1140-1196
CeCl <sub>3</sub>	2.2677	31788	340.4	251.3	1090 - 1177
PrCl <sub>3</sub>	2.0054	34087	338.9	244.7	1064-1185
NdCl <sub>3</sub>	2.09865	33605	352.4	255.7	1025 - 1151
PmCl <sub>3</sub>	1.9549	35000	356.9	255.5	_
SmCl <sub>3</sub>	1.5362	38823	360.4	248.7	948-1094
EuCl <sub>3</sub>	1.8502	35000	321.4	230.1	_

this is not the first evidence of somewhat unusual behaviour of molten LaCl<sub>3</sub>. Molar electrical conductivity of molten LaCl<sub>3</sub> is a little lower and activation energy of the electricity transport is higher as follows from the common tendency (see Figure 2 in [20], Figures 12, 14 in [21]). Lower conductivity is easy explained due to higher viscosity of this melt. In thermophysical studies [22-24], and references therein] authors point to reproducible hysteresis between enthalpies of melting and crystallization. They attribute this phenomenon to the postmelting effect with the formation of particular chain-like structure of liquid. Similar ideas have already been proposed by Savin et al. [25, 26]. According to [27-31] the average coordination number of  $La^{3+}$  ions is essentially higher (7-8) as compared with other  $Ln^{3+}$  ions (typically 6 [32, 33]). The higher is the coordination number the higher is the viscosity and the lower is the conductance.

**PmCl<sub>3</sub>**. Promethium was not available in any form to the authors for investigation in this study. According to analysis of electronic structure of  $Pm^{3+}$  ion [34], the properties of molten  $PmCl_3$  should closely fall in common tendencies in properties changes from LaCl<sub>3</sub> to LuCl<sub>3</sub>. In this sense NdCl<sub>3</sub> is the closest analogue of  $PmCl_3$ . The estimation of viscosity of molten  $PmCl_3$  made by interpolation is included in Tables 1-3 and illustrated in Figures 3 and 6.

**EuCl<sub>3</sub>**. It is not possible to measure the viscosity of molten EuCl<sub>3</sub> in the same manner as that of other chlorides because of its thermal decomposition. The most reliable estimation of EuCl<sub>3</sub> melting point is  $632 \degree C$  [34]. Appreciable decomposition begins at  $400-500\degree C$  and of course essentially increases un-

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der reduced pressure. Furthermore, molten and solid EuCl<sub>3</sub>, as a rule, exhibit physical and chemical properties lying outside of general tendency [20, 35]. Electrical conductivity of molten EuCl<sub>3</sub> is higher by 20% approximately as follows from common tendency in lanthanide row. The fact was well established in papers [35, 36] and confirmed by our independent measurements [20, 37]. EuCl<sub>3</sub> is a single salt with one type of cations  $(Eu^{3+})$  and one type of anions  $(Cl^{-})$ . Higher conductivity of molten EuCl<sub>3</sub> in comparison with neighbouring SmCl<sub>3</sub> and GdCl<sub>3</sub> can be the consequence of looser structure of the melt. Looser structure leads to higher mobility of ions, thus to larger conductivity and also to lower viscosity. The idea that high conductivity arises due to partial thermal decomposition of EuCl<sub>3</sub> with formation of more mobile Eu<sup>2+</sup> cations is unfounded. Electrical conductance of molten  $EuCl_3 - EuCl_2$  system has been measured over all composition range [20, 37]. A partial EuCl<sub>3</sub> decomposition ranging 5-10% leads to increasing of conductivity only by 2.8 - 5.7 %.

To a first approximation the viscosity of molten  $EuCl_3$  is taken also lower about by 20% as follows from the tendency, see Figures 3 and 6 and Tables 1–3.

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Supplementary Tab	<b>bles.</b> Kinematic viscosities <i>v</i>	$n^2/s$ of molten r	rare earth chlorides. Initial data.
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	$\frac{1}{1} \begin{bmatrix} 1 \\ 0 \end{bmatrix} \begin{bmatrix} 1 \\ $	Exp. 25 5).
	804.3 1.329 810.3 1.342 841.9 1.168 871.5 1.052 901.8 0.9649	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	804.3 1.344 823.3 1.230 852.2 1.162 882.7 1.002 901.9 0.9361	
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	803.9 1.329 823 1.270 852.5 1.091 882 1.017 901.2 0.9506	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	804 1.323 823 1.232 852.3 1.116 882.4 1.026 901.6 0.9630	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	804 1.316 823.2 1.232 852.3 1.101 882.6 0.9923 901.5 0.9617	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	793.9 1.356 830 1.163 852.2 1.113 890.8 0.9950 911.2 0.9335	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	793 1.366 829.8 1.217 862 1.094 891 0.9838 911.5 0.9354	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	792.7 1.378 829.8 1.248 862.1 1.095 889.8 0.9925 912 0.9203	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	792.8 1.394 829.5 1.196 861 1.110 890 1.0000 912.2 0.9085	
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	792.6 1.394 841.8 1.133 872.8 1.050 889.7 0.9682 911.6 0.9479	
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	809.8 1.301 841.7 1.131 872.8 1.047 889.9 0.9925	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	<u>810.9</u> <u>1.278</u> <u>842.2</u> <u>1.159</u> <u>873.1</u> <u>1.041</u> <u>890.4</u> <u>0.9920</u>	
$\begin{array}{c c c c c c c c c c c c c c c c c c c $		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$t [^{\circ}C]  v \cdot 10^{-6}  t [^{\circ}C]  v \cdot 10^{-6}  Table 6. PrCl_3 (v + 1)^{-6}  t [^{\circ}C]  v \cdot 10^{-6}  v \cdot 10^{-6}  t [^{\circ}C]  v \cdot 10^{-6}  t [^{\circ}C]  v \cdot 10^{-6}$	Exp. 23-7).
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	806.7 1.374 829 1.256 831.1 1.229 818.2 1.287 814.2 1.313	
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	797.2 1.391 829.7 1.243 818.2 1.287 814.4 1.317	
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	791.1 1.437 831 1.246 818.2 1.282 813.9 1.312	
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$		
848.8       1.208       811.8       1.322       837       1.218       850.8       1.162       881.4       1.079       13).         833.3       1.233       811.3       1.326       836.2       1.246       851       1.197       881.4       1.092         833.4       1.239       801.1       1.375       836.3       1.228       850.4       1.197       883.3       1.085         833.2       1.241       800.4       1.390       836.1       1.253       851       1.163       891.5       1.057         833.5       1.253       800.3       1.391       836.2       1.244       861.8       1.147       890.7       1.061         833.4       1.260       800.8       1.404       835.5       1.253       861.3       1.153       889.4       1.042         833.2       1.260       791.2       1.428       835.7       1.231       861.3       1.153       889.4       1.044         823.3       1.302       791.3       1.444       835.7       1.231       861.8       1.141       889.8       1.046         824       1.285       841.2       1.208       851.3       1.165       862       1.143       889.3	$\frac{t [^{\circ}C] + v \cdot 10^{-6} + t [^{\circ}C] + v \cdot 10^{-6}}{t [^{\circ}C] + v \cdot 10^{-6} + t [^{\circ}C] + v \cdot$	(Exp. 23-
833.3       1.233       811.3       1.326       836.2       1.246       851       1.197       881.4       1.092         833.4       1.239       801.1       1.375       836.3       1.228       850.4       1.197       883.3       1.085         833.2       1.241       800.4       1.390       836.1       1.253       851       1.163       891.5       1.057         833.5       1.253       800.3       1.391       836.2       1.224       861.8       1.147       890.7       1.061         833.4       1.260       800.8       1.404       835.6       1.249       862.9       1.130       890       1.042         833.2       1.260       791.2       1.428       835.5       1.253       861.3       1.153       889.4       1.044         823.3       1.302       791.3       1.444       835.7       1.231       861.8       1.141       889.8       1.046         824       1.285       841.2       1.208       851.3       1.165       862.5       1.073       904.4       1.019         823.6       1.291       840.4       1.201       850.5       1.198       882.5       1.084       904       1.01	<u>848.8</u> <u>1.208</u> <u>811.8</u> <u>1.322</u> <u>837</u> <u>1.218</u> <u>850.8</u> <u>1.162</u> <u>881.4</u> <u>1.079</u> <u>13</u> ).	
833.4       1.239       801.1       1.375       836.3       1.228       850.4       1.197       883.3       1.085         833.2       1.241       800.4       1.390       836.1       1.253       851       1.163       891.5       1.057         833.5       1.253       800.3       1.391       836.2       1.224       861.8       1.147       890.7       1.061         833.4       1.260       800.8       1.404       835.6       1.249       862.9       1.130       890       1.042         833.2       1.260       791.2       1.428       835.5       1.253       861.3       1.153       889.4       1.044         823.3       1.302       791.3       1.444       835.7       1.231       861.8       1.141       889.8       1.046         824       1.285       841.2       1.208       851.3       1.165       862       1.143       889.3       1.062         823.6       1.291       840.4       1.201       850       1.162       882.5       1.073       904.4       1.019         823.5       1.298       840.6       1.209       850.5       1.198       882.5       1.084       904       1.012<	833.3 1.233 811.3 1.326 836.2 1.246 851 1.197 881.4 1.092	
833.2       1.241       800.4       1.390       836.1       1.253       851       1.163       891.5       1.057         833.5       1.253       800.3       1.391       836.2       1.224       861.8       1.147       890.7       1.061         833.4       1.260       800.8       1.404       835.6       1.249       862.9       1.130       890       1.042         833.2       1.260       791.2       1.428       835.5       1.253       861.3       1.153       889.4       1.044         823.3       1.302       791.3       1.444       835.7       1.231       861.8       1.141       889.8       1.046         824       1.285       841.2       1.208       851.3       1.165       862       1.143       889.3       1.062         823.6       1.291       840.4       1.201       850       1.162       882.5       1.073       904.4       1.019         823.5       1.298       840.6       1.209       850.5       1.198       882.5       1.084       904       1.012	833.4 1.239 801.1 1.375 836.3 1.228 850.4 1.197 883.3 1.085	
833.5       1.253       800.3       1.391       836.2       1.224       861.8       1.147       890.7       1.061         833.4       1.260       800.8       1.404       835.6       1.249       862.9       1.130       890       1.042         833.2       1.260       791.2       1.428       835.5       1.253       861.3       1.153       889.4       1.044         823.3       1.302       791.3       1.444       835.7       1.231       861.8       1.141       889.8       1.046         824       1.285       841.2       1.208       851.3       1.165       862       1.143       889.3       1.062         823.6       1.291       840.4       1.201       850       1.162       882.5       1.073       904.4       1.019         823.5       1.298       840.6       1.209       850.5       1.198       882.5       1.084       904       1.012	833.2 1.241 800.4 1.390 836.1 1.253 851 1.163 891.5 1.057	
833.4       1.260       800.8       1.404       835.6       1.249       862.9       1.130       890       1.042         833.2       1.260       791.2       1.428       835.5       1.253       861.3       1.153       889.4       1.044         823.3       1.302       791.3       1.444       835.7       1.231       861.8       1.141       889.8       1.046         824       1.285       841.2       1.208       851.3       1.165       862       1.143       889.3       1.062         823.6       1.291       840.4       1.201       850       1.162       882.5       1.073       904.4       1.019         823.5       1.298       840.6       1.209       850.5       1.198       882.5       1.084       904       1.012	833.5 1.253 800.3 1.391 836.2 1.224 861.8 1.147 890.7 1.061	
833.2       1.260       791.2       1.428       835.5       1.253       861.3       1.153       889.4       1.044         823.3       1.302       791.3       1.444       835.7       1.231       861.8       1.141       889.8       1.046         824       1.285       841.2       1.208       851.3       1.165       862       1.143       889.3       1.062         823.6       1.291       840.4       1.201       850       1.162       882.5       1.073       904.4       1.019         823.5       1.298       840.6       1.209       850.5       1.198       882.5       1.084       904       1.012	833.4 1.260 800.8 1.404 835.6 1.249 862.9 1.130 890 1.042	
823.3       1.302       791.3       1.444       835.7       1.231       861.8       1.141       889.8       1.046         824       1.285       841.2       1.208       851.3       1.165       862       1.143       889.3       1.062         823.6       1.291       840.4       1.201       850       1.162       882.5       1.073       904.4       1.019         823.5       1.298       840.6       1.209       850.5       1.198       882.5       1.084       904       1.012	833.2 1.260 791.2 1.428 835.5 1.253 861.3 1.153 889.4 1.044	
824       1.285       841.2       1.208       851.3       1.165       862       1.143       889.3       1.062         823.6       1.291       840.4       1.201       850       1.162       882.5       1.073       904.4       1.019         823.5       1.298       840.6       1.209       850.5       1.198       882.5       1.084       904       1.012	823.3 1.302 791.3 1.444 835.7 1.231 861.8 1.141 889.8 1.046	
823.6 1.291 840.4 1.201 850 1.162 882.5 1.073 904.4 1.019 823.5 1.298 840.6 1.209 850.5 1.198 882.5 1.084 904 1.012	824 1.285 841.2 1.208 851.3 1.165 862 1.143 889.3 1.062	
823.5 1.298 840.6 1.209 850.5 1.198 882.5 1.084 904 1.012	823.6 1.291 840.4 1.201 850 1.162 882.5 1.073 904.4 1.019	
	823.5 1.298 840.6 1.209 850.5 1.198 882.5 1.084 904 1.012	
823.5 1.285 840.5 1.202 850.7 1.180 881.3 1.072 904.3 1.015	823.5 1.285 840.5 1.202 850.7 1.180 881.3 1.072 904.3 1.015	
811.6 1.348 840.7 1.208 850.8 1.189 881.9 1.087	811.6 1.348 840.7 1.208 850.8 1.189 881.9 1.087	

**Note 1.** Final equation for kinematic viscosity of molten  $PrCl_3$  (Table 1 in the main text) was computed as an average of equations, calculated from data of Exp. 23-5, Exp. 23-7, and Exp. 23-13, at that the equation after Exp. 23-7 was taken with weight 1/2.